**Transient-Free Operations With Physics-Based Real-time Analysis and Control**

# **Egemen Kolemen**

**David Eldon, Alex Glasser, Alan Glasser, John Ferron, Bill Eggert, K. Burrell, David Humphreys, Orso Meneghini**

**Mechanical & Aerospace Engineering Jointly appointed with the Andlinger Center for Energy and the Environment and the Plasma Physics Laboratory (PPPL)**







This work supported in part by U.S. Department of Energy under DE-SC0015878 and DE-FC02-04ER54698.

andlinger center for energy+the environmen

## **Real-time Stability Calculations for Plasma Control and Disruption Avoidance**



- **For cost-effective commercial fusion power plants to be feasible, we need to operate close to stability limits**
- **There must also be almost no disruption in fusion power reactors and very few disruptions in ITER**
- **This necessitates real-time stability analysis for plasma control and disruption avoidance**







1611-00446/3 **E. Kolemen / San Jose / Nov 2016**





1611-00446/4 **E. Kolemen / San Jose / Nov 2016**





1611-00446/5 **E. Kolemen / San Jose / Nov 2016**





1611-00446/6 **E. Kolemen / San Jose / Nov 2016**



1611-00446/7 **E. Kolemen / San Jose / Nov 2016**

## **Real-time Computational Analysis for Fusion Adds New Challenges**

- **In order to produce real-time stability computation useful for control, we need to:**
- **1. >>99% reliability**
	- **Use a well known analysis and tested codes** è **Ideal MHD**
- **2. Take the physicist out of the loop**
	- **Automated Real-time Kinetic Equilibrium reconstruction**



#### **1. Real-Time Kinetic Equilibrium Reconstruction**

#### **2. Real-time Stability Calculations**



#### **Real Time Kinetic Equilibrium Reconstruction Will be Implemented by Adding P and J Constraints to EFIT**

• EFIT solves the Grad-Shafranov Equation

$$
\Delta^* \psi = -\mu_0 R^2 p' - \mu_0^2 f f' \qquad \qquad \frac{R \partial Z}{J_z = \frac{1}{R} \frac{\partial f}{\partial R}}
$$

 $I_{\rm B} = -\frac{1}{\pi} \frac{\partial f}{\partial x}$ 

- $\psi$  constrained by magnetics
- *J* constrained by magnetics and MSE



#### **Real Time Kinetic Equilibrium Reconstruction Will be Implemented by Adding P and J Constraints to EFIT**

• EFIT solves the Grad-Shafranov Equation

$$
\Delta^* \psi = -\mu_0 R^2 p' - \mu_0^2 f f'
$$
\n
$$
J_R = -\frac{1}{R} \frac{\partial f}{\partial Z}
$$
\n
$$
J_Z = \frac{1}{R} \frac{\partial f}{\partial R}
$$

- $\psi$  constrained by magnetics
- *J* constrained by magnetics and MSE

#### **Additional constraints in a kinetic EFIT: New**

- $\boldsymbol{p}$  is constrained by TS, CER, and fast ion calculations
- *J* is further constrained by  $J_{BS} + J_{OHM} + J_{ECCD}$ calculations



## **With David Eldon and John Ferron**

#### **Real Time Kinetic Equilibrium Reconstruction Difference between regular versus kinetic-EFIT**



• **Pedestal pressure gradient and the resulting bootstrap current introduces errors throughout the profiles**

• **Critical to constrain equilibria for stability** 



#### **Real-time Thomson Working at DIII-D**



• **We acquire the Thomson data in real-time.**



• **Calibrate and fit it** è **Input to auto-kefit**

1611-00446/13 **E. Kolemen / San Jose / Nov 2016**

#### **RT-CER constraints on the Current and Pressure**





• **Core CER channels already acquired** 

• **Edge CER chords for pedestal are added this year**

• **Calibration and fitting for getting Ion temperature and density are to be tested this run campaign**

#### **Fast Ion Approximation Tool (FIAT) provides quick access to fast ion profiles (Bill Eggert)**



• **Fast ion pressure:**

### • *FIAT* **surveys 1000s of shots**

- Read fast ion profiles from ONETWO results
- Fit fast ion profiles w/ Gaussian & record amplitude and width
- $\rightarrow$  **Fast function for estimating fast ion profiles then can be used in realtime**



#### **Add soft constraints on the Current and Pressure to RT EFIT**



• **RT-Thomson (two years ago), RT-CER (this year)**



#### **auto\_kEFIT is Built on the Assumption that There is No User Input During the Workflow (David Eldon)**



- **Offline Testing Started** è **Online Development**
- **Pick your shot & timing and press GO!**
- **Aim: No Human Intervention requirement**



#### **The developer interface with one GO button**

#### **1. RT-Kinetic EFIT**

#### **2. Real-time Stability Calculations**



1611-00446/18 **E. Kolemen / San Jose / Nov 2016**

## **How can we achieve rt-Stability calculations (Alex Glasser)**

### • **Need for Control:**

#### – Two time scales of crucial importance are

- Energy confinement time, $\tau_F$ ,  $\rightarrow$  pressure profile to equilibrate
- Current relaxation time, $\tau_{R}$ ,  $\rightarrow$  plasma current density profile to equilibrate
- In DIII–D,  $\tau_F \sim 200$  ms &  $\tau_R$  is  $\sim 2$  s, in ITER both  $>$  seconds.

#### • **How to get it:**

- The fastest Stability Calculations: Single core DCON 5 s for *n*=1 and 10 s for *n*=2.
- Parallelizing DCON
	- Parallelize the coordinate transfer
	- Parallelize into subdomains (ODE)
- $-$  Initial results show we can get to  $\sim$ 200 ms computation time



## **Stability Analysis: Using RT-EFIT + DCON**

- **Start with non-resistive DCON with the wall**
- Start with non-resistive DCON with the wall<br>• Solves the ideal MHD (low toroidal number)
- **Using the Energy Principle**

$$
\delta W = \frac{1}{2} \int_{\Omega} d\mathbf{x} \left[ Q^2 + \mathbf{J} \cdot \boldsymbol{\xi} \times \mathbf{Q} + (\boldsymbol{\xi} \cdot \nabla P)(\nabla \cdot \boldsymbol{\xi}) + \gamma P (\nabla \cdot \boldsymbol{\xi})^2 \right]
$$

■ The  $\Xi_{\psi}$  which minimizes the 'action'  $\delta W_P$  is seen to satisfy the Euler-Lagrange equation:

$$
\left(\mathbf{F}\Xi^{\prime}_{\psi}+\mathbf{K}\Xi_{\psi}\right)^{\prime}-\left(\mathbf{K}^{\dagger}\Xi^{\prime}_{\psi}+\mathbf{G}\Xi_{\psi}\right)=0
$$

• **Convert the problem to a 2-point BVP (with analyticity condition at singular points) because it allows fast computation methods**

$$
\left.\begin{pmatrix}\dot{\mathbf{q}}\\\dot{\mathbf{p}}\end{pmatrix}\right\vert=\mathbf{A}(\psi)\begin{pmatrix}\mathbf{q}\\ \mathbf{p}\end{pmatrix}\text{ with } \mathbf{q}(0)=0,\ \mathbf{p}(1)=0,\text{ and }\mathbf{K}^{\dagger}\mathbf{F}^{-1}\mathbf{K}\mathbf{q}\right\vert_{m_{s}}=0
$$

## **Parallelize integration for multiple cores with state transition matrix and domain decomposition**





## **Parallelize integration for multiple cores with state transition matrix and domain decomposition**



1611-00446/22

## **Parallelize integration for multiple cores with state transition matrix and domain decomposition**





### **Integration at singular surface (1)**

• **State transition matrices may be inverted to integrate out from singular surfaces rather than in, ensuring only analytic solutions are integrated**

$$
\boldsymbol{\Phi}^{-1}(\psi_1,\psi_2) = \boldsymbol{\Phi}(\psi_2,\psi_1)
$$





#### **Integration at singular surface (2)**

• **State transition matrices may be inverted to integrate out from singular surfaces rather than in, ensuring only analytic solutions are integrated**



1611-00446/25

## **Vision: Real-time Stability Calculations for Plasma Control and Disruption Avoidance**



- **Develop the system for ITER on current machines**
- **Each server will run a different variation of a profile parameter (e.g. increase NBI power, reduce edge current etc.)**
- **Project the stability in the future.**
- **If approaching stability boundary change/control the profiles**
	- Calculate multiple profile variations  $\rightarrow$  choose the best path

1611-00446/26 **E. Kolemen / San Jose / Nov 2016 (Kim and Lister NF 2012)** 

#### **Conclusions**

- **Automated kinetic equilibrium reconstructions is implemented at DIII-D → Real-time under development**
- **Real-time methods for ideal stability calculations based on DCON are under development at DIII-D**
- **Aim: Control profiles evolution to keep the plasma away form the stability boundaries**
	- **First to be tested at DIII-D**
	- **Then, implemented at ITER**



This report was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor any agency thereof, nor any of their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise, does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or any agency thereof. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or any agency thereof.